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Presented for filing is a new original patent application of:

Applicant: ROGER PANICACCI; BARMAK MANSOORIAN; SANDOR
BARNA; ALEXANDER I. KRYMSKI
Title: READOUT CIRCUIT WITH GAIN AND
ANALOG-TO-DIGITAL CONVERSION FOR IMAGE
SENSOR

Enclosed are the following papers, including those required to receive a filing date
under 37 CFR §1.53(b):

	<u>Pages</u>
Specification	36
Claims	12
Abstract	1
Declaration	2
Drawing(s)	16

Enclosures:

- Small entity statement. This application is entitled to small entity status.
- Assignment cover sheet and an assignment, 4 pages, and a separate \$40.00 fee.

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Valentin Figner

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March 8, 1999

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- New disclosure information, including:
Information disclosure statement, 1 page.
PTO-1449, 2 pages.
References, 7 items.
- Postcard.

Basic filing fee	380.00
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Fee for multiple dependent claims	0.00
Total filing fee:	\$ 650.00

A check for the total filing fee is enclosed. Please apply any other required fees or any credits to deposit account 06-1050, referencing the attorney docket number shown above.

Under 35 U.S.C. § 119(e)(1), this application claims the benefit of U.S. Provisional Patent Application No. 60/077,599, filed March 9, 1998.


If this application is found to be incomplete, or if a telephone conference would otherwise be helpful, please call the undersigned at 212/765-5070.

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Respectfully submitted,


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49578.N11

Applicant or Patentee: Roger Panicacci; Barmak Mansoorian; Sandor Barna; Alexander I. Krymski
 Serial or Patent No.:
 Filed or Issued:
 For:

READOUT CIRCUIT WITH GAIN AND ANALOG-TO-DIGITAL CONVERSION FOR IMAGE SENSOR

VERIFIED STATEMENT (DECLARATION) CLAIMING SMALL ENTITY STATUS
 (37 CFR 1.9(f) and 1.27(c)) - SMALL BUSINESS CONCERN

I hereby declare that I am

- ☐ the owner of the small business concern identified below;
☒ an official of the small business concern empowered to act on behalf of the concern identified below:

Name of Small Business Concern: Photobit Corporation

Address of Small Business Concern: 135 North Los Robles Avenue, 7th Floor, Pasadena, CA 91101

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READOUT CIRCUIT WITH GAIN AND ANALOG-TO-DIGITAL CONVERSION FOR IMAGE SENSOR

by inventor(s) Roger Panicacci; Barmak Mansoorian; Sandor Barna; and Alexander I. Krymski described in

- ☒ the specification filed herewith.
☐ application serial no. , filed .
☐ patent no. , issued .

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Date: 3/8/99

APPLICATION

FOR

UNITED STATES LETTERS PATENT

TITLE: READOUT CIRCUIT WITH GAIN AND ANALOG-TO-DIGITAL
CONVERSION FOR IMAGE SENSOR

APPLICANTS: ROGER PANICACCI; BARMAK MANSOORIAN; SANDOR
BARNA; and ALEXANDER I. KRYMSKI

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Valentin Figueroa

VALENTIN FIGUEROA

READOUT CIRCUIT WITH GAIN AND ANALOG-TO-DIGITAL CONVERSION
FOR IMAGE SENSOR

5

BACKGROUND

This disclosure relates, in general, to image sensors and, in particular, to readout circuits for such sensors.

Image sensors find applications in a wide variety of
10 fields, including machine vision, robotics, guidance and navigation, automotive applications, and consumer products. In many smart image sensors, it is desirable to integrate on-chip circuitry to control the image sensor and to perform signal and image processing on the output image. Unfortun-
15 ately, charge-coupled device (CCD), which have been one of the dominant technologies used for image sensors, do not easily lend themselves to large scale signal processing and are not easily integrated with CMOS circuits. Moreover, a CCD is read out by sequentially transferring the signal
20 charge through the semiconductor, and the readout rate is limited by the need for nearly perfect charge transfer.

Active pixel sensors (APS), which have one or more active transistors within the pixel unit cell, can be made compatible with CMOS technologies and promise higher readout
25 rates compared to passive pixel sensors. Active pixel sensors are often arranged as arrays of elements, which can be read out, for example, a column at a time. As it is read

out, each column is driven and buffered for sensing by a readout circuit.

The analog signals that are read out from the sensor array typically are converted to digital signals to

5 facilitate subsequent processing of the image. During analog-to-digital conversion, a reference voltage can be used to generate digital representations of the analog input signals. Signal resolution often is maximized when the expected range of the analog input signal matches the

10 reference voltage level. However, in some situations, the output of the CMOS image sensor has a relatively low voltage level due to a low light condition or operation at a high frame rate. Thus, in such situations, it may be necessary or desirable to amplify the output signals from the CMOS
15 image sensor to provide a stronger analog input signal to the analog-to-digital converter (ADC).

In some imagers, a single readout stage is used to an entire array of pixels. Recently, there has been heightened interest in parallel column architectures to
20 increase the overall speed and/or accuracy of the output stage. However, in the past, size and power constraints have limited the extent to which such architectures could be implemented for a CMOS imager.

SUMMARY

In general, according to one aspect, a circuit for reading out values of pixels from an active pixel sensor array includes a first sample-and-hold circuit for sampling and storing signals from pixels in a first column and a second sample-and-hold circuit for sampling and storing signals from pixels in a second column. An operational amplifier-based charge sensing circuit, associated with only the first and second columns in the array, selectively provides an amplified differential output signal based on signals sampled either by the first sample-and-hold circuit or the second sample-and-hold circuit.

The readout circuit also can include an analog-to-digital converter, associated only with the first and second columns in the array, for converting the differential output to a corresponding digital signal using a successive approximation technique.

In various implementations, one or more of the following features are present. For example, a pre-gain offset voltage selectively can be added to a signal sampled by one of the sample-and-hold circuits. Furthermore, the readout circuit can include an array of capacitors which selectively can be enabled to choose a gain associated with the operational amplifier-based charge sensing circuit. In some embodiments, the circuit has first and second arrays of

capacitors which selectively can be enabled to choose a gain associated with the operational amplifier-based charge sensing circuit. One array can be used to select the gain with respect to signals sampled by the first sample-and-hold circuit, and the second array can be used to select the gain with respect to signals sampled by the second sample-and-hold circuit. Additionally, the operational amplifier-based charge sensing circuit can include a switched capacitor integrator.

The analog-to-digital converter can include, for example, a comparator and a first binary-scaled capacitor network. In one embodiment, the capacitors in the first network share a common node coupled to a first input of the comparator, and the amplified differential output signal from the charge sensing circuit is coupled to a second input of the comparator. Each of the capacitors in the first capacitor network can have an associated latch circuit. The latch circuit can store a bit corresponding to a differential signal for a pixel sampled by the first sample-and-hold circuit while a differential signal for a pixel sampled by the second sample-and-hold circuit is amplified and converted to a corresponding digital signal.

The readout circuit further can include a calibration network for providing a signal to cancel an offset of the comparator. A second binary-scaled capacitor

network can be used to successively approximate and store the offset of the comparator, and the capacitors in the second capacitor network can share a node in common with the capacitors in the first capacitor network. In some

5 implementations, the calibration network selectively can be enabled to provide a DC shift to the common node to ensure that the signal for cancelling the comparator offset appears as a positive voltage. In one particular embodiment, one side of each capacitor in the first capacitor network
10 selectively can be connected to a first reference voltage, and one side of each capacitor in the second capacitor network selectively can be connected to a second reference voltage different from the first reference voltage. In some implementations, the calibration network selectively can be
15 enabled to provide a post-gain offset for the differential output signal from the charge sensing circuit.

According to another aspect, a CMOS imager includes an array of active pixel sensors, where each pixel is associated with a respective column in the array. The

20 imager also has multiple circuits for reading out values of pixels from the active sensor array. Each readout circuit is associated with a respective pair of first and second columns in the array. In addition, each circuit includes a first sample-and-hold circuit for sampling and storing
25 signals from pixels in the first column and a second sample-

and-hold circuit for sampling and storing signals from pixels in the second column. Each readout circuit also includes a respective operational amplifier-based charge sensing circuit that selectively provides an amplified differential output signal based on signals sampled either by the first sample-and-hold circuit or the second sample-and-hold circuit. Furthermore, each readout circuit has an analog-to-digital converter for converting the differential output to a corresponding digital signal using a successive approximation technique.

In other implementations, each readout circuit can be associated with only a single column of sensors rather than two columns. In other words, each column would have its own respective amplification and analog-to-digital conversion stages. In yet other implementations, a single amplification stage and analog-to-digital conversion stage can be associated with a group of more than two columns (e.g, four or six) in the array.

According to another aspect, a method of reading out values from active pixel sensors in an array of sensors includes selecting a row of sensors whose values are to be read out and sampling signal and reset levels for two sensors in the selected row. A differential output signal is provided based on the sampled signals for a selected one of the sensors using an operational amplifier-based charge

sensing circuit associated with only the two columns in which the two sensors are located. The differential output signal then is converted to a corresponding digital signal using an analog-to-digital converter associated with only
5 the two columns.

In some implementations, a pre-gain offset voltage to a sampled signal can be provided. Similarly, a gain can be selected for the differential output signal. In some cases, the act of converting the signal from an analog to a
10 digital signal includes using a successive approximation technique, and a signal can be provided to cancel a comparator offset. The analog-to-digital conversion also can include providing a DC voltage shift to ensure that the signal for cancelling the comparator offset appears as a
15 positive voltage. In some implementations, a post-gain offset is provided for the differential output signal.

In the present description, the functions performed with respect to columns and rows of pixels in an array can be reversed. Accordingly, a reference to a column in a two-
20 dimensional pixel sensor array should be understood as referring to one or more pixel sensors along one axis of the array, and a reference to a row in the array should be understood as referring to one or more pixel sensors along a second axis of the array, where the second axis is
25 orthoganol to the first axis.

Various implementations include one or more of the following advantages. For example, a readout circuit with a variable gain and analog-to-digital conversion can be made sufficiently small, compact and low-powered so that a

5 separate readout circuit can be provided for each column or pair of columns of pixels in an array. Use of the readout circuit, therefore, can increase the parallel structure of the overall chip, thereby reducing the bandwidth which the circuit must be capable of handling.

10 Sampling both the reset and signal levels allows correlated double sampling (CDS) to be performed which can reduce various forms of noise from the pixel. Furthermore, sensing charge using an operational amplifier-based integrator circuit allows the pixel values to be read out at
15 a relatively high rate. In addition, the calibration network can help provide more accurate results by correcting various offsets associated with the circuitry and by extending the dynamic range of the analog-to-digital converter

20 Other features and advantages will be readily apparent from the following description, accompanying drawings and the claims.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of an exemplary CMOS active pixel sensor chip.

FIG. 2 is a block diagram showing an array of active pixel sensors and a parallel column readout stage for providing amplification and analog-to-digital conversion.

FIG. 3 is a block diagram illustrating further details of a readout circuit with amplification and analog-to-digital conversion.

FIG. 4 is an embodiment of the readout circuit.

FIG. 5 is a timing diagram for sample and hold steps associated with the circuit of FIG. 4.

FIG. 6 is a circuit diagram of an exemplary operational amplifier for use in the circuit of FIG. 4.

FIG. 7 is a timing diagram for an amplification step associated with the circuit of FIG. 4.

FIG. 8 is a circuit diagram of an exemplary comparator for use in the circuit of FIG. 4.

FIG. 9 is a timing diagram illustrating a process of successive approximation performed during analog-to-digital conversion.

FIG. 10 is an exemplary logic circuit associated with the analog-to-digital conversion.

FIG. 11 is a timing diagram associated with the circuit of FIG. 10.

FIG. 12 is an exemplary logic circuit associated with a calibration network for the analog-to-digital conversion.

FIG. 13 is a timing diagram associated with the
5 circuit of FIG. 12.

FIG. 14 is another embodiment of the readout circuit.

FIGS. 15 and 16 are timing diagrams associated with the circuit of FIG. 14.

10 DETAILED DESCRIPTION

FIG. 1 shows an exemplary CMOS active pixel sensor integrated circuit chip that includes an array of active pixel sensors 30 and a controller 32 which provides timing and control signals to enable reading out of signals stored
15 in the pixels. Exemplary arrays have dimensions of 128 by 128 pixels or 256 by 256 pixels, although, in general, the size of the array 30 will depend on the particular implementation. The imager is read out a row at a time using a parallel column readout architecture. The
20 controller 32 selects a particular row of pixels in the array 30 by controlling the operation of a vertical addressing circuit 34 and row drivers 40. Signals stored in the selected row of pixels are read out to circuitry 42 for amplifying the pixel signals and for converting the analog

signals to corresponding digital signals. Signals for selecting the digital signals corresponding to a particular column in the array are provided from the controller 32 through a horizontal addressing circuit 44.

5 FIG. 2 shows the array 30 with multiple columns, 49A through 49N, of CMOS active pixel sensors 50. Each column includes multiple rows of sensors 50. Signals from the active pixel sensors 50 can be read out to respective circuits 52 each of which is associated with a different group of one or more columns 49A through 49N, with each column associated with one of the circuits 52. As shown in FIG. 3, each of the circuits 52 can receive and process signals from a pair of columns. For example, one of the circuits 52 receives and processes signals from columns 49A and 49B. In other implementations, each circuit 52 may receive and process signals either from only a single column or from more than two columns of sensors. For example, in some implementations, each circuit 52 would receive and process signals from four columns. Digital signals
10
15
20 corresponding to the analog pixel signals then can be read out serially to a bus 54.

As shown in FIG. 3, according to one implementation, each circuit 52 includes circuits 60A, 60B for sampling and holding signals from a corresponding one of the columns of pixels. For example, the circuit 60A can sample and hold
25

signals from the column 49A, and the circuit 60B can sample and hold signals from the column 49B. In particular, pixel signal and reset values can be sampled by each of the sample-and-hold circuits 60A, 60B so as to generate a double
5 sampled differential value. Additional circuitry 62A, 62B allows a pre-gain offset voltage VREF4 to be added or subtracted to a reset signal stored by the sample-and-hold circuits 60A, 60B.

The circuit 52 further includes an analog
10 multiplexer (MUX) which allows the differential value corresponding to a selected one of the pixels to be passed through to a charge transimpedance amplifier (CTIA) 66 which can have a variable gain. The amplified differential signal is stored by another sample-and-hold circuit 68 and is
15 provided to a summing node 70. The summing node 70 also receives signals from a calibration network 72 which uses reference voltages VREF2, VREF3. The output of the summing node 70 is provided to an analog-to-digital converter (ADC) 74 which uses a reference voltage (VREF1). One or more
20 latches 76 store the digital bits and can be enabled to transmit the bits to the bus 54.

As shown in FIG. 4, CMOS active pixel sensors 50A, 50B are located in respective columns 49A, 49B of the sensor array. Each sensor 50A, 50B can include a photo-sensitive
25 element 80 buffered by a source-follower transistor 82 and a

row selection switch which can be implemented by a transistor 84. A signal "ROW" is applied to the gate of the row selection transistor 84 to enable a particular row of pixels. In one implementation, the element 80 includes a photogate with a floating diffusion output separated by a transfer gate. Each pixel 50A, 50B also includes a reset switch which can be implemented as a transistor 86 controlled by a signal "RST" applied to its gate.

As further illustrated in FIG. 4, the readout circuit 52 includes load transistors M1, M2 for the respective source-followers 82. As described in greater detail below, signals from selected pixels can be read into the respective sample-and-hold circuits 60A, 60B. The two sample-and-hold circuits 60A, 60B are substantially the same and, thus, only one of them will be described in detail.

The sample-and-hold circuit 60A includes a sample switch S1 and a charge storage element such as the capacitor C1. The switch S1 can be implemented as a transistor which can be enabled to be in a conductive state or a non-conductive state.

A pre-gain offset voltage can be added to a value stored by the capacitor C1 by controlling the states of switches S6, S7 which connect the lower plate of a capacitor C2 either to ground or to the offset voltage VREF4. The capacitor C2 is connected in parallel with the capacitor C1.

The capacitor C2 can be used, for example, to subtract a dark signal level prior to amplifying the pixel signal. That can increase the dynamic range of the sensor 50 by removing a common DC offset from the pixel array 30.

5 Preferably, the ratio of the values of the capacitors C2 and C1 is approximately 1 to 64.

A source-follower transistor M3 with a load transistor M4 is coupled between the hold capacitor C1 and an array of clamping capacitors C3, C4, C5 connected in
10 parallel. In one implementation, the capacitors C3, C4, C5 form a binary-scaled array. Thus, for example, the values of C3, C4 and C5 can be 64, 128 and 256 femto-farads, respectively. Each capacitor in the array has a corresponding switch S2, S3, S4. When a switch, such as the
15 switch S2, is closed, one of its poles is coupled to the right-hand plate of the corresponding capacitor C3. A second pole of each switch S2, S3, S4 can be coupled to a clamping voltage level Vcl by closing a switch S5.

To provide a signal from a selected one of the
20 sample-and-hold circuits 60A, 60B to the amplifier circuit 66, one of two switches S8, S9 is closed. For example, to select the output of the circuit 60A, the switch S8 would be closed. Conversely, to select the output of the circuit 60B, the switch S9 would be closed. Thus, the switches S8,
25 S9 correspond to the multiplexer 64 in FIG. 3. Each of the

switches S2 through S9 can be implemented, for example, as transistors which can be switched between a conductive and non-conductive state by applying appropriate voltage signals to their respective gates.

5 The operation of the sample-and-hold circuits 60A, 60B is explained with reference to the timing diagram of FIG. 5. During signal integration in the pixel array 30, the row selection transistors 84 are turned off by setting the row selection signal "ROW" to a low signal such as 0
10 volts (V). Following signal integration, an entire row of pixels is read out substantially simultaneously with pixels from two columns being sampled by each circuit 52.

 Prior to reading out the row of pixels, the switches S2, S3, S4 and S5 are closed. At this time, the switches
15 S8, S9 should be open. Next, the pixels in the row to be read out are addressed by enabling the corresponding row selection transistors 84. Thus, the signal value on the photosensitive element 80 in the pixel 50A is switched through the corresponding source-follower transistor 82 and
20 row selection transistor 84. The sampled pixel value is held by the capacitor C1 in the sample-and-hold circuit 60A. Similarly the left-hand plates of the capacitors C3, C4, C5 are held at the pixel signal value. The right-hand plates of the clamping capacitors C3, C4, C5 are held at the
25 voltage level Vcl. At substantially the same time, the

signal value of the pixel 50B appears on the corresponding array of capacitors in the sample-and-hold circuit 60B.

Next, the switch S5 in each sample-and-hold circuit 60A, 60B is opened so that the right-hand plates of the capacitors C3, C4, C5 remain floating at the voltage level Vc1. The photosensitive element 80 in each pixel in the selected row is reset by enabling the corresponding reset transistor 86. The reset level of the pixel then is stored by the corresponding capacitor C1. Similarly, the voltage on the floating side of the clamping capacitors C3, C4, C5 rises above the voltage level Vc1 by an amount equal to the difference between the pixel reset level (V_{reset}) and the signal level (V_{signal}). The sample switch S1 is then opened.

Once the pixel signal and reset values have been sampled, the differential values are amplified, and the amplified values are converted to corresponding digital signals. Since the two sample-and-hold circuits 60A, 60B share a single gain and analog-to-digital conversion circuit, the amplification and conversion steps are performed with respect to the pixel from the even-numbered column (e.g., column 49A) and subsequently performed for the pixel from the odd-numbered column (e.g., column 49B). A set of latches 96 associated with the ADC 74 stores the results from the first amplification and conversion steps while the pixel value from the remaining column is being

processed. Then, two bytes of information corresponding to the two pixels 50A, 50B are read out from the latches 96 to transfer the bytes to the bus 54, with one byte transferred during each clock cycle.

Returning to FIG. 4, further details of the charge sensing amplifier circuit 66 are now explained. The amplifier circuit 66 includes an operational amplifier 90, a feedback switch S10 and a feedback capacitor C6. Details of an exemplary operational amplifier 90 are illustrated in FIG. 6. The gain (G) of the charge sensing amplifier circuit 66 is determined by the clamping capacitors C3, C4, C5 (FIG. 4) that are selectively coupled to an input of the operational amplifier 90 through the switch S8 (or S9). The gain of the amplifier circuit is, therefore, approximately equal to the ratio of the effective capacitance seen by the negative terminal of the operational amplifier 90 and the value of the feedback capacitor C6. Thus, the gain (G) can be varied by closing a selected one or more of the switches S2, S3, S4 during the amplification step.

The output of the operational amplifier 90 is coupled through a switch S14 to a circuit that includes capacitors C8, C9, C10. A clamping circuit includes a switch S15 that selectively can be closed to hold the right-hand plate of the capacitor C10 at the voltage level V_{cl} . A source-follower transistor M7 with a load transistor M6

couples the output of the operational amplifier 90 to the capacitors C9, C10.

The amplifier circuit 66 also can include additional circuitry for reducing or eliminating an offset of the operational amplifier 90. The additional circuitry includes the capacitor C7 and switches S11, S12, S13, with common poles of the switches S11 and S13 held at the reference voltage Vcl. Each of the switches S10 through S15 can be implemented, for example, as transistors which can be switched between a conductive and non-conductive state by applying appropriate voltage signals to their respective gates.

Operation of the amplification stage of the circuit 52 is explained with reference to the timing diagram of FIG. 7. The operational amplifier 90 is reset by closing the switch S10, at which time the switches S11 and S12 also are closed. The offset of the operational amplifier 90 is stored across the capacitor C7 connected to the positive terminal. At substantially the same time, the clamping circuit is enabled to store the offset level by closing the switches S14 and S15.

Next, the reset switch S10, as well as the switches S11, S12, are opened, and the switch S13 is closed. In addition, the clamping switch S15 is opened. As a result, the offset of the operational amplifier 90 is stored on its

positive terminal, and the output of the operational amplifier settles to about the voltage level V_{cl} . The clamping capacitor C10 stores the reset value of the operational amplifier 90 relative to the voltage level V_{cl} .

5 While the reset operation is being performed, one or more of the switches S2, S3, S4 are closed to select the variable gain (G) of the amplifier circuit. In some applications, the same gain is used for all the pixels. In other applications, however, the sensor array is configured
10 to capture color images by covering different pixels with different spectrum-discriminating filters. Each pixel responds to a different primary color, such as red, green or blue. Different gains may be applied to signals from pixels associated with different colors which can be desirable, for
15 example, to increase the perceived luminance of the captured image.

Once the reset operation for the operational amplifier 90 has been completed, the switch S8 (or S9) is closed to enable the charge stored on the clamping
20 capacitors C3, C4 and/or C5 to be transferred to the feedback capacitor C6. The signal appearing at the output of the operational amplifier 90 is proportional to the gain (G) times the difference between the pixel reset and signal levels ($V_{reset} - V_{signal}$). When the switch S14 at the output
25 of the operational amplifier 90 is opened, the voltage at

the left-hand plate of the clamping capacitor C10 is the amplified differential signal relative to the voltage level Vc1.

The amplified differential analog signal then is converted to a corresponding digital signal by the ADC 74. In the implementation of FIG. 4, the ADC 74 includes a comparator 92 and a binary-scaled network of capacitors C11, C12, C18. Details of an exemplary comparator circuit 92 are illustrated in FIG. 8. The comparator 92 includes positive and negative terminals and an output. A "strobe" signal enables the comparator 92 to provide an output signal based on the signals at its positive and negative terminals.

The binary-scaled capacitor network is used to approximate the amplified differential pixel signal using a successive approximation technique. The capacitor C11 corresponds to the most significant bit (MSB) in the digital signal, whereas the capacitor C18 corresponds to the least significant bit (LSB). The relationship between the values of the capacitors for adjacent bits is such that the capacitance corresponding to the more significant bit is twice the capacitance of the less significant bit. Thus, if the capacitor C11 has a capacitance of C, the capacitor C12 would have a capacitance of C/2. In one implementation, the capacitor network includes eight capacitors so that the analog differential signal can be converted to an 8-bit

digital signal. The capacitor C18 would then have a capacitance of $C/2^7$.

The bottom plate of each capacitor C11, C12, C18 can be connected to either zero volts or a reference voltage VREF1 by using respective switches S17, S18 associated with the particular capacitor. The reference voltage VREF1 defines the dynamic range of the ADC 74. Each of the capacitors C11, C12, C18 in the network has associated logic 94 and a latch 96 for storing one of the eight bits corresponding to the digital value for the pixel. Details of an exemplary circuit for the logic 94 and latch 96 are illustrated in FIG. 10.

Prior to the analog-to-digital conversion step, the binary-scaled capacitor network is reset. For example, the capacitor network can be reset while the amplification step is being performed. To reset the capacitor network, a clamping switch S16 (FIG. 4) is closed to connect the common upper plate of the capacitors C11 through C18 to the voltage Vcl. The switches S17 associated with the capacitors C11 through C18 also are closed to connect the lower capacitor plates to zero volts. By the time the amplification step is completed, the binary-scaled capacitor network is ready for the analog-to-digital conversion process, at which time the switch S16 is open.

To determine the corresponding digital value of the differential pixel signal, the bottom plate of the largest capacitor C11, corresponding to the most significant bit, is switched to the reference voltage VREF1 by closing the switch S18 associated with that capacitor. The resulting voltage level on the common upper plate of the capacitor network appears on the negative terminal of the comparator 92, and the differential analog pixel signal appears at the positive terminal of the comparator. If the voltage level on the negative terminal of the comparator 92 is greater than the value of the differential pixel signal, then the ADC 74 is returned to its initial value by switching the bottom plate of the capacitor C11 back to zero volts, which corresponds to a digital low bit ("0"). On the other hand, if the voltage level on the negative terminal of the comparator 92 is less than the value of the differential pixel signal, then the bottom plate of the capacitor C11 is kept at the reference voltage VREF1, which corresponds to a digital high bit ("1").

The foregoing set of operations is repeated for the remaining capacitors in the binary-scaled network in order of size. The ADC 74, therefore, adjusts the voltage appearing on the negative terminal of the comparator 92 in increments of $VREF1/2$, $VREF1/4$, etc, in order to approximate the value of the differential pixel signal. As the

algorithm proceeds, the voltage appearing on the negative terminal of the comparator 92 approaches the differential pixel signal until it is equal to it, within the precision of the ADC 74 (see FIG. 9).

5 The result of the comparison for each capacitor C11 through C18 in the binary-scaled network is stored by the associated one of the latches 96 to hold the switches S17, S18 in their proper positions. Once the foregoing operations are completed for each of the capacitors C11
10 through C18 in the binary scaled network, the values of the digital bits corresponding to the analog differential pixel signal are stored by the respective latches 96 while the amplification and conversion steps are performed for the pixel 50B from the odd-numbered column 49B.

15 Operation of the circuitry for the logic 94 and latch 96 is described with respect to one of the capacitors in the binary-scaled capacitor network, for example, the capacitor C11, with reference to FIG. 10 and the timing diagram of FIG. 11. The circuit of FIG. 10 includes two
20 latches 96A, 96B each of which has a tri-state driver. Prior to enabling the comparator 92, the circuit of FIG. 10 is cleared by asserting a "clear" signal to turn on the transistor M5. A "preset_bar" signal is asserted which sets a first latch 96A and causes a transistor M7, which
25 corresponds to the switch S18 in FIG. 4 to be turned on.

The lower plate of the capacitor C11 is, thus, connected to the voltage level VREF1. Then, the comparator 92 is enabled by asserting the "strobe" signal (see FIG. 8). The output of the comparator 92, is provided to the transistor M6, and
5 a "select" signal enables a transistor M9 to allow the comparator output signal to be locked into the latch 96A.

If the output from the comparator 92 is low, then the transistor M7 remains enabled and the lower plate of the capacitor C11 remains connected to the voltage level VREF1.

10 On the other hand, if the comparator output is high, then the transistor M8, corresponding to the switch S17 in FIG. 4, is turned on, thereby connecting the lower plate of the capacitor C11 to ground. The foregoing operations are performed in sequence with respect to each of the capacitors
15 C11 through C18 so as to determine and store a value for each of the eight bits.

Next, the latched values corresponding to the eight bits for the pixel are transferred to the respective second latches 96B while the analog value of the pixel 50B is
20 amplified and converted to its corresponding digital value. The transfer operation is performed in parallel for all eight bits. Prior to transferring the digital bit stored by each latch 96A to the corresponding latch 96B, a "pre2bar" signal is asserted to set the latch 96B. The "pre2bar"
25 signal can be asserted at about the same time as the "clear"

signal discussed above. A "transfer_enable" signal is asserted to transfer the value stored by the first latch 96A to the second latch 96B.

Once the bits corresponding to the differential value for the pixel 50A have been transferred to the latches 96B, the operational amplifier 90 can be reset, and the amplification and conversion processes are repeated with respect to the differential signal for the pixel 50B. The eight bits corresponding to the pixel 50B would then be stored in the latches 96A. A "col_select_bar" signal then is provided from the addressing circuit 44 (FIG. 1) to the latches 96 to read out the two bytes of information. In one implementation, the amplification process and the analog-to-digital conversion process take approximately ten microseconds each.

Returning now to FIG. 4, the circuit 52 also includes a calibration network 72 to provide corrections for the analog-to-digital conversion based, for example, on the offset of the comparator 92. The calibration network 72 also includes a network of capacitors C19, C24, C25, C26 whose upper plates are electrically connected to the upper plates of the capacitors C11, C12, C18 in the ADC binary-scaled network. Each capacitor C19, C24, C25 and C26 has a respective latch and logic associated with it. For example, the capacitors C19, C24 have respective latches 102 and

logic 100 associated with them and can be connected to either zero volts or a reference voltage VREF2. Similarly, the capacitor C25 has a latch 106 controlled by logic 104 associated with it and can be connected to either zero volts or the reference voltage VREF2. The capacitor C26 has a latch 110 and controlled by logic 108 associated with it and can be connected to either zero volts or a reference voltage VREF3.

The capacitors C19, C24 form a binary-scaled network similar to the network formed by the capacitors C11 through C18, with the capacitor C19 representing a most significant bit (MSB) and the capacitor C24 representing the least significant bit (LSB). Although only two capacitors are shown, the binary-scaled network in the calibration network 72 can include additional capacitors. Thus, in one implementation, the binary-scaled network in the calibration network 72 has five capacitors, such that if the value of the capacitor C19 is C, then the value of the capacitor C24 would be C/16. The set of capacitors C19 through C24 are used to help reduce fixed pattern noise (FPN) as described below.

Calibration can be performed, for example, when power is initially applied to the active sensor pixel chip. In general, the calibration is performed by applying substantially the same voltage to both the positive and

negative terminals of the comparator 92, using the binary-scaled capacitor network (C19 through C24) to approximate the value at the output of the comparator, and storing the comparator offset in the calibration network 72. More specifically, the clamping capacitor C10 is charged to the voltage Vcl, and the voltage Vcl is provided to both the positive and negative terminals of the comparator 92 by closing the clamping switches S15 and S16. Initially, the capacitors C19 through C26 in the calibration network 72 are connected to zero volts. The binary-scaled capacitor network (C19 through C24) then can be used to successively approximate the comparator offset in a manner similar to the technique described above with respect to the binary-sealed capacitor network in the ADC 74. The estimated value of the comparator offset is stored by the respective latches 102 and can be applied to the common upper plate of the capacitors in the ADC binary-scaled network just prior to the conversion process using an "enable_offset" signal (see FIG. 11). That has the effect of cancelling the comparator offset in the analog domain before the analog-to-digital conversion begins.

The reference voltage VREF2 used by the binary-scaled network in the calibration network 72 should be separate from the reference voltage VREF1 used by the binary-scaled network in the ADC 74 because the reference

voltage for the conversion bits can change depending on the environment. Using separate reference voltages eliminates the need to recalibrate each time the reference voltage for the ADC changes. In addition, using a separate reference
5 voltage enables sub-LSB offset correction of the comparator 92.

An exemplary circuit for the logic 100 and latch 102 associated with each of the capacitors, C19 through C24, is illustrated in FIG. 12. Operation of the circuitry for the
10 logic 100 and latch 102 is described with respect to one of the capacitors in the binary-scaled capacitor network, for example, the capacitor C19, with reference to FIG. 12 and the timing diagram of FIG. 13. The circuit of FIG. 12 initially is cleared by asserting a "cclr" signal which
15 turns on the transistor M10, thereby connecting the capacitor C19 to ground through the transistor M11. The transistor M11 corresponds to the switch S19 in FIG. 4.

Once the capacitor C10 at the positive terminal of the comparator 92 is charged to the voltage Vc1, the
20 "enable_offset" signal is asserted, thereby turning on the transistors M12, M13. Next, a signal "cpreset_bar" is asserted which turns on a transistor M14. That, in turn, causes the transistor M11 to be turned off, and the transistor M15, which correspond to the switch S20 in FIG.

4, to be turned on. The lower plate of the capacitor C19 is, thus, connected to the voltage VREF2.

Next, the comparator 92 is enabled by asserting the "strobe" signal (see FIG. 8). The output of the comparator 92 is provided to the transistor M16, and a "cselect" signal enables a transistor M17 to allow the comparator output signal to be locked into the latch 102. If the output from the comparator 92 is low, then the transistor M16 is disabled. The transistor M11 remains turned off, and the transistor M15 remains turned on so that the lower plate of the capacitor C19 remains connected to VREF2. On the other hand, if the comparator output is high, then the transistor M15 is turned off and the transistor M11 is turned on, thereby connecting the lower plate of the capacitor C19 to ground. The foregoing operations are performed in sequence with respect to each of the capacitors C19 through C24 so as to determine and store the offset value of the comparator 92 in the calibration network 72.

As previously noted, the comparator offset stored by the calibration network 72 can be applied to the common upper plate of the capacitors in the ADC binary-scaled network just prior to the conversion process by asserting the "enable_offset" signal (see FIG. 11) to cancel the comparator offset.

In the implementation of FIG. 4, the analog-to-digital architecture does not determine a sign bit for the comparator offset. Thus, one of the additional capacitors (C25) in the calibration network 72 can be used during the calibration process to add a DC shift to ensure that the comparator offset appears as a positive voltage and is within the range that is established by the voltage level VREF2. The value of the capacitor C25 should be at least as large as the largest capacitor in the binary-scaled correction network (C19 through C24). In other words, the value of the capacitor C25 should be at least as large as the value of the capacitor C19.

The capacitor C26 in the calibration network 72 can be used to add a post-gain offset voltage to the differential pixel value to increase the dynamic range of the ADC 74. The post-gain offset can help eliminate, for example, the clipping of very small signals due to systematic ADC offsets. The value of the capacitor C26 can be the same as the capacitor C19.

FIG. 14 illustrates an alternative embodiment of the readout circuit 52. Components that are the substantially the same as in the embodiment of FIG. 4 are identified by the same reference numbers or letters. The circuit 52 of FIG. 14 differs primarily with respect to the configuration of the sample-and-hold circuits 60A, 60B, the circuits 62A,

62B that provides the pre-gain offset, and the amplification circuit 66. As in the implementation of FIG. 4, the circuit 52 samples values from pixels in two columns in parallel and then processes them sequentially.

5 In FIG. 14, each sample-and-hold circuit, such as the sample-and-hold circuit 60A, includes a first switch, implemented as transistor M30, and a capacitor C30. A signal (SHS) is applied to the gate of the transistor M30 to control whether the transistor is in a conductive or non-
10 conductive state. The sample-and-hold circuit also includes a second switch, implemented as transistor M31, and a capacitor C31. A signal (SHR) is applied to the gate of the transistor M31 to control the state of the transistor. This arrangement allows both the pixel signal and reset values to
15 be sampled and stored. Thus, correlated double sampling (CDS) can be performed to reduce reset noise associated with the pixel as well as noise associated with the source-follower transistor 82. Signals stored by the capacitors C30, C31 can be provided to a source-follower transistor M34
20 by enabling a respective one of the switches M32, M33. A signal "phi_s0" controls the state of the switch M32, whereas a signal "phi_r0" controls the state of the switch M33.

The operation of the sample-and-hold circuit 60A in
25 FIG. 14 is explained with reference to the timing diagram of

FIG. 15. A sampled pixel value is switched through the sampling transistor M30 to one side of the capacitor C30 by asserting the signal "shs." Next, the pixel 50A is reset by asserting the signal "RST" and the reset value is switched
5 through the sampling transistor M31 to one side of the capacitor C31 by asserting the signal "shr".

A variable pre-gain offset can be provided to the sampled reset value using the circuitry 62A which includes multiple capacitors C32, C33, C34 connected in parallel each
10 of which can be connected either to ground or to the reference voltage (VREF4) using respective switches S30, S31, S32.

The sample-and-hold circuit 60B and the associated circuitry 60B for establishing a pre-gain offset with
15 respect to the odd column can be identical to the corresponding circuit for the even column. Once the signal and reset values for the pixels 50A, 50B have been sampled and stored, the amplification and analog-to-digital conversion steps are performed for the even-column pixel 50A
20 and subsequently for the odd-column pixel 50B.

The amplification stage 66 of the circuit in FIG. 14 includes the operational amplifier 90, the reset switch S10 which is controlled by a signal "phi_rst," and the feedback capacitor C6. The amplification circuit 66 also includes a
25 binary-scaled array of capacitors C35 through C39 which

allows a variable gain to be selected. The left-hand plate of each capacitor C35 through C39 is connected to a common node at the output of the source-follower transistor M34. The right-hand plate of each of the capacitors C35 through C39 can be connected to the negative terminal of the operational amplifier by closing respective switches S35 through S39.

In contrast to the configuration of FIG. 4, the circuitry for correcting the offset of the operational amplifier 90 can be eliminated in FIG. 14, and the positive terminal of the operational amplifier can be connected directly to the voltage Vcl. Similarly, in the implementation of FIG. 14, only a single capacitor array for establishing the variable gain is needed, in contrast to the two capacitor arrays (C3, C4, C5) used in the implementation of FIG. 4.

The operation of the amplification stage of the circuit of FIG. 14 is explained with reference to the timing diagram of FIG. 16. A "node_reset" signal on the gate of a transistor M35 is asserted to clear any residual charge remaining on the common line at the input to the source-follower M34. The operational amplifier 90 is reset by asserting the signal "phi_rst" to close the reset switch S10. At substantially the same time, the variable gain is selected by closing one or more of the switches S35 through

S39, and a signal "phi_out" is asserted to close the switch S14 at the output of the operational amplifier 90.

The pixel reset value stored, for example, by the capacitor C31 in the sample-and-hold circuit 60A is driven to the left-hand plates of the capacitors C35 through C39 by asserting a signal "phi_ro" which closes the switch M33.

The right-hand plate of the clamping capacitor C10 at the output stage of the operational amplifier 90 is charged to the voltage Vc1 by asserting the signal "CL2" to close the

switch S15. The reset switch S10 for the operational amplifier 90 then is turned off, and once the output of the operational amplifier 90 settles to the voltage Vc1, the switch S15 also is turned off.

Next, the switch M33 is turned off. The switch M32 then can be turned on by asserting a signal "phi_so" to drive the pixel signal level stored by the capacitor C30 to the array of capacitors C35 through C39. The charge is transferred to the feedback capacitor C6, which causes the output of the operational amplifier 90 to increase by the gain (G) times the differential value between the pixel reset and signal values. The amplified differential value also appears at the clamping capacitor C10.

Once the amplification step is complete, the amplified differential value can be converted to a corresponding digital value in the manner described above

with respect to FIG. 4. The entire process can be repeated with respect to the reset and signal values corresponding to the pixel 50B from the odd column and previously stored by the sample-and-hold circuit 60B. As previously described, the two bytes of information corresponding to the pixels 50A, 50B can be transferred to the bus 54, with one byte transferred during each clock cycle.

The foregoing implementations have been explained assuming that the pixels 50A, 50B operate in a photodiode mode in which the pixel signal value is sampled prior to the pixel reset value. However, in other implementations, the pixels can operate in a photogate mode in which the reset value is sampled prior to the signal value.

Additionally, the foregoing implementations have been described with respect to a column parallel architecture in which each readout circuit 52 processes signals from two columns. However, as previously mentioned, the readout circuits 52 can be modified so that each readout circuit is associated with only a single column of sensors, In that case, each readout circuit would need only one of the sample-and-hold circuits 60A, 60B. Similarly, each latch circuit 96 could be simplified because it would need to store just a single bit for the particular pixel signal being processed.

In other implementations, a single amplification stage and analog-to-digital conversion stage can be associated with a group of columns (e.g, four or six) in the array. In such a situation, the readout circuit would
5 include multiple sample-and-hold circuits according to the number of columns with which the amplification and analog-to-digital stages are associated.

Other implementations are within the scope of the following claims.

10

What is claimed is:

1. A circuit for reading out values of pixels from an active pixel sensor array, the circuit comprising:

a first sample-and-hold circuit for sampling and storing signals from pixels in a first column;

5 a second sample-and-hold circuit for sampling and storing signals from pixels in a second column; and

an operational amplifier-based charge sensing circuit, associated with only the first and second columns in the array, that selectively provides an amplified

10 differential output signal based on signals sampled either by the first sample-and-hold circuit or the second sample-and-hold circuit.

2. The circuit of claim 1 further including an array of capacitors which selectively can be enabled to

15 choose a gain associated with the operational amplifier-based charge sensing circuit.

3. The circuit of claim 1 further including:

a first array of capacitors which selectively can be enabled to choose a gain associated with the

20 operational amplifier-based charge sensing circuit with respect to signals sampled by the first sample-and-hold circuit; and

a second array of capacitors which selectively
can be enabled to choose a gain associated with the
operational amplifier-based charge sensing circuit with
respect to signals sampled by the second sample-and-hold
5 circuit.

4. The circuit of claim 1 wherein a pre-gain
offset voltage selectively can be added to a signal sampled
by one of the sample-and-hold circuits.

5. The circuit of claim 1 wherein the
10 operational amplifier-based charge sensing circuit includes
a switched capacitor integrator.

6. A circuit for reading out values of pixels
from an active pixel sensor array, the circuit comprising:
a sample-and-hold circuit for sampling and
15 storing signals from sensors in a single column of pixels in
the array; and

an operational amplifier-based charge sensing
circuit, associated with only the single column in the
array, that provides an amplified differential output signal
20 based on signals sampled by the sample-and-hold circuit.

7. The circuit of claim 6 further including an array of capacitors which selectively can be enabled to choose a gain associated with the operational amplifier-based charge sensing circuit.

5 8. A circuit for reading out values of pixels from an active pixel sensor array, the circuit comprising:

a first sample-and-hold circuit for sampling and storing signals from pixels in a first column;

a second sample-and-hold circuit for sampling and storing signals from pixels in a second column;

10 an operational amplifier-based charge sensing circuit, associated only with the first and second columns in the array, that selectively provides an amplified differential output signal based on signals sampled either by the first sample-and-hold circuit or the second sample-and-hold circuit; and

15 an analog-to-digital converter, associated only with the first and second columns in the array, for converting the differential output to a corresponding digital signal using a successive approximation technique.

9. The circuit of claim 8 wherein the operational amplifier-based charge sensing circuit includes a switched capacitor integrator.

10. The circuit of claim 8 wherein the analog-to-digital converter includes a comparator and a first binary-scaled capacitor network, wherein the capacitors in the first network share a common node coupled to a first
5 input of the comparator, and wherein the amplified differential output signal from the charge sensing circuit is coupled to a second input of the comparator.

11. The circuit of claim 10 wherein each of the capacitors in the first capacitor network has an
10 associated latch circuit for storing a bit corresponding to a differential signal for a pixel sampled by the first sample-and-hold circuit while a differential signal for a pixel sampled by the second sample-and-hold circuit is amplified and converted to a corresponding digital signal.

12. The circuit of claim 10 further including:
15 a calibration network for providing a signal to cancel an offset of the comparator.

13. The circuit of claim 12 further including:
20 a second binary-scaled capacitor network used to successively approximate and store the offset of the comparator, wherein the capacitors in the second capacitor

network share a node in common with the capacitors in the first capacitor network.

14. The circuit of claim 13 wherein the calibration network selectively can be enabled to provide a DC shift to the common node to ensure that the signal for cancelling the comparator offset appears as a positive voltage.

15. The circuit of claim 13 wherein one side of each capacitor in the first capacitor network selectively can be connected to a first reference voltage, and wherein one side of each capacitor in the second capacitor network selectively can be connected to a second reference voltage different from the first reference voltage.

16. The circuit of claim 13 wherein the calibration network selectively can be enabled to provide a post-gain offset for the differential output signal from the charge sensing circuit.

17. A circuit for reading out values of pixels from an active pixel sensor array, the circuit comprising:

a sample-and-hold circuit for sampling and storing signals from sensors in a single column of pixels in the array;

an operational amplifier-based charge sensing circuit, associated with only the single column, that provides an amplified differential output signal based on signals sampled by the sample-and-hold circuit; and

an analog-to-digital converter, associated only with only the single column, for converting the differential output to a corresponding digital signal using a successive approximation technique.

18. A CMOS imager comprising:

an array of active pixel sensors, wherein each pixel is associated with a respective column in the array;

and

a plurality of circuits for reading out values of pixels from the active sensor array, wherein each readout circuit is associated with a respective pair of first and second columns in the array, and wherein each circuit

includes:

a first sample-and-hold circuit for sampling and storing signals from pixels in the first column;

a second sample-and-hold circuit for
sampling and storing signals from pixels in the second
column;

an operational amplifier-based charge
5 sensing circuit that selectively provides an amplified
differential output signal based on signals sampled either
by the first sample-and-hold circuit or the second sample-
and-hold circuit; and

an analog-to-digital converter for
10 converting the differential output to a corresponding
digital signal using a successive approximation technique.

19. The imager of claim 18 wherein each readout
circuit further includes an array of capacitors which
selectively can be enabled to choose a gain associated with
15 the operational amplifier-based charge sensing circuit.

20. The imager of claim 18 wherein each readout
circuit further includes:

a first array of capacitors which selectively
can be enabled to choose a gain associated with the
20 operational amplifier-based charge sensing circuit with
respect to signals sampled by the first sample-and-hold
circuit; and

a second array of capacitors which selectively
can be enabled to choose a gain associated with the
operational amplifier-based charge sensing circuit with
respect to signals sampled by the second sample-and-hold
5 circuit.

21. The imager of claim 18 wherein, for each
readout circuit, a pre-gain offset voltage selectively can
be added to a signal sampled by one of the sample-and-hold
circuits.

10 22. The imager of claim 18 wherein, for each
readout circuit, the operational amplifier-based charge
sensing circuit includes a switched capacitor integrator.

23. The imager of claim 18 wherein, for each
readout circuit, the analog-to-digital converter includes a
15 comparator and a first binary-scaled capacitor network,
wherein the capacitors in the first network share a common
node coupled to a first input of the comparator, and wherein
the amplified differential output signal from the charge
sensing circuit is coupled to a second input of the
20 comparator.

24. The imager of claim 23 wherein, for each readout circuit, each of the capacitors in the first capacitor network has an associated latch circuit for storing a bit corresponding to a differential signal for a pixel sampled by the first sample-and-hold circuit while a differential signal for a pixel sampled by the second sample-and-hold circuit is amplified and converted to a corresponding digital signal.

25. The imager of claim 24 wherein the latch circuits in each readout circuit also can store bits corresponding to a differential signal for a pixel sampled by a respective one of the second sample-and-hold circuits, wherein the imager further includes a bus, and wherein the latch circuits in a particular readout circuit selectively can be enabled to transfer the bits to the bus.

26. The imager of claim 23 wherein each readout circuit further includes:

a calibration network for providing a signal to cancel an offset of the comparator.

27. The imager of claim 26 wherein each readout circuit further includes:

a second binary-scaled capacitor network used to successively approximate and store the offset of the comparator, wherein the capacitors in the second capacitor network share a node in common with the capacitors in the first capacitor network.

28. The imager of claim 27 wherein, for each readout circuit, the calibration network selectively can be enabled to provide a voltage shift to the common node to ensure that the signal for cancelling the comparator offset appears as a positive voltage.

29. The imager of claim 27 wherein, for each readout circuit, one side of each capacitor in the first capacitor network selectively can be connected to a first reference voltage, and wherein one side of each capacitor in the second capacitor network selectively can be connected to a second reference voltage different from the first reference voltage.

30. The imager of claim 27 wherein, for each readout circuit, the calibration network selectively can be enabled to provide a post-gain offset for the differential output signal from the charge sensing circuit.

31. A method of reading out values from active pixel sensors in an array of sensors, wherein the array includes rows and columns of sensors, the method comprising:

5 selecting a row of sensors whose values are to be read out;

 sampling signal and reset levels for two sensors in the selected row;

 providing a differential output signal based on the sampled signals for a selected one of the sensors using
10 an operational amplifier-based charge sensing circuit associated with only the two columns in which the two sensors are located;

 converting the differential output signal to a corresponding digital signal using an analog-to-digital
15 converter associated with only the two columns.

32. The method of claim 31 further including providing a pre-gain offset voltage to a sampled signal.

33. The method of claim 31 further including selecting a gain for the differential output signal.

20 34. The method of claim 31 wherein the act of converting includes using a successive approximation technique.

35. The method of claim 31 wherein the act of converting includes providing a signal to cancel a comparator offset.

36. The method of claim 35 wherein the act of
5 converting further includes providing a DC voltage shift to ensure that the signal for cancelling the comparator offset appears as a positive voltage.

37. The method of claim 31 further including
providing a post-gain offset for the differential output
10 signal.

ABSTRACT

A CMOS imager includes an array of active pixel sensors, wherein each pixel is associated with a respective column in the array. The imager also includes multiple circuits for reading out values of pixels from the active sensor array. Each readout circuit can be associated with a respective pair of columns in the array and can include first and second sample-and-hold circuits. The first and second sample-and-hold circuits are associated, respectively, with first and second columns of pixels in the array. Each readout circuit also includes an operational amplifier-based charge sensing circuit that selectively provides an amplified differential output signal based on signals sampled either by the first sample-and-hold circuit or the second sample-and-hold circuit. The readout circuit also has an analog-to-digital converter for converting the differential output to a corresponding digital signal using a successive approximation technique. Use of the readout circuit can increase the parallel structure of the overall chip, thereby reducing the bandwidth which each readout circuit must be capable of handling.

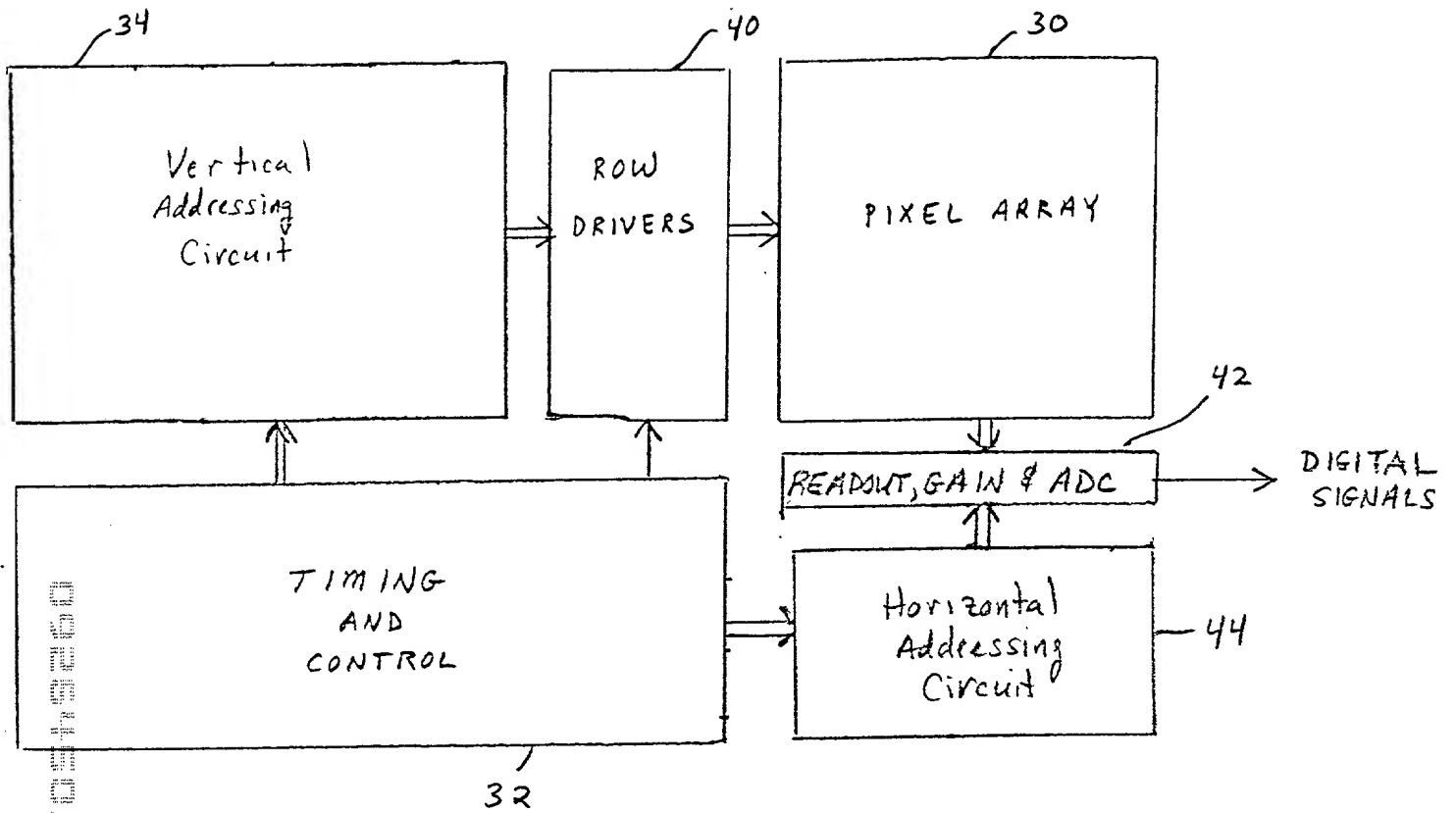


FIG. 1

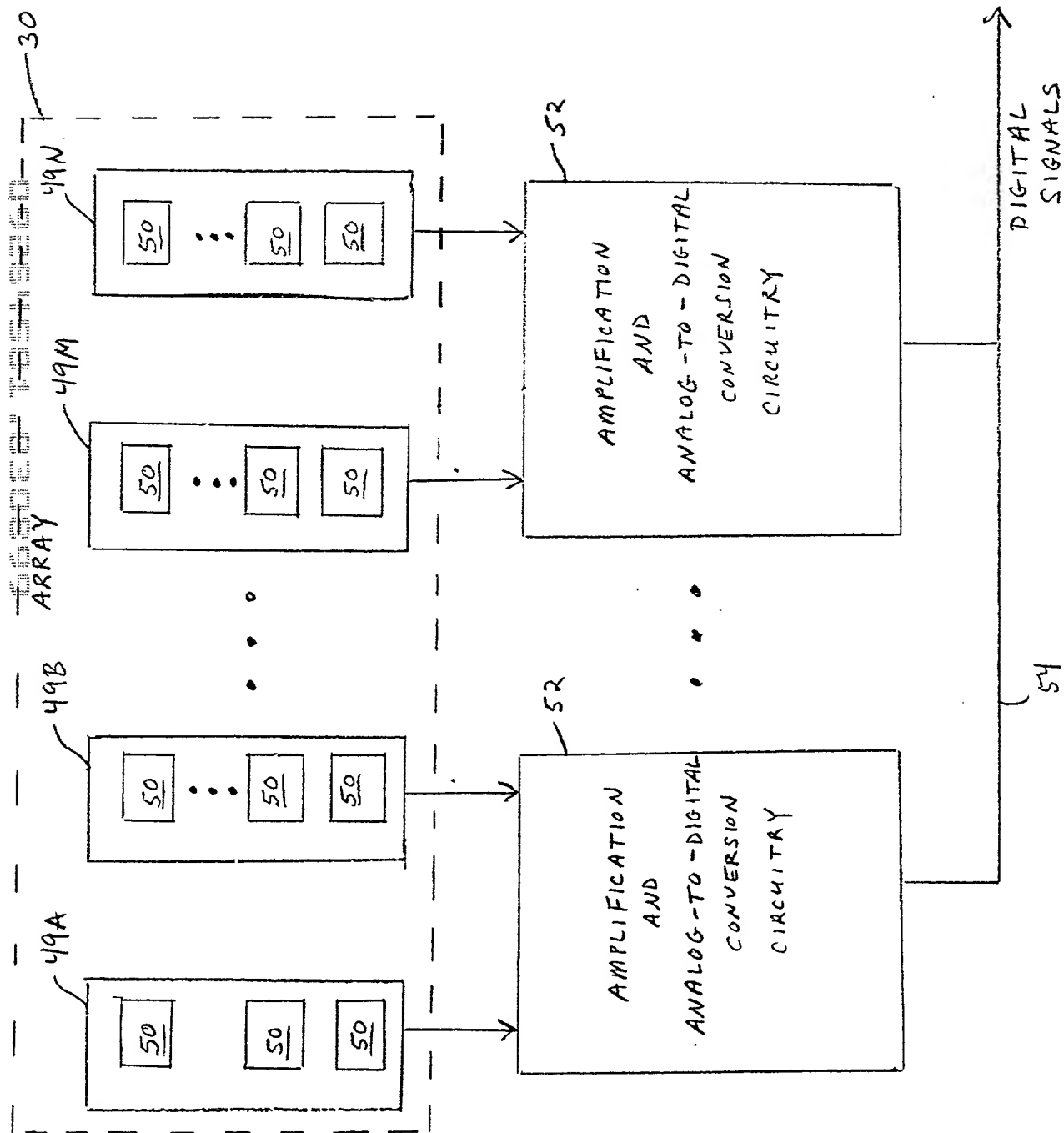


FIG. 2

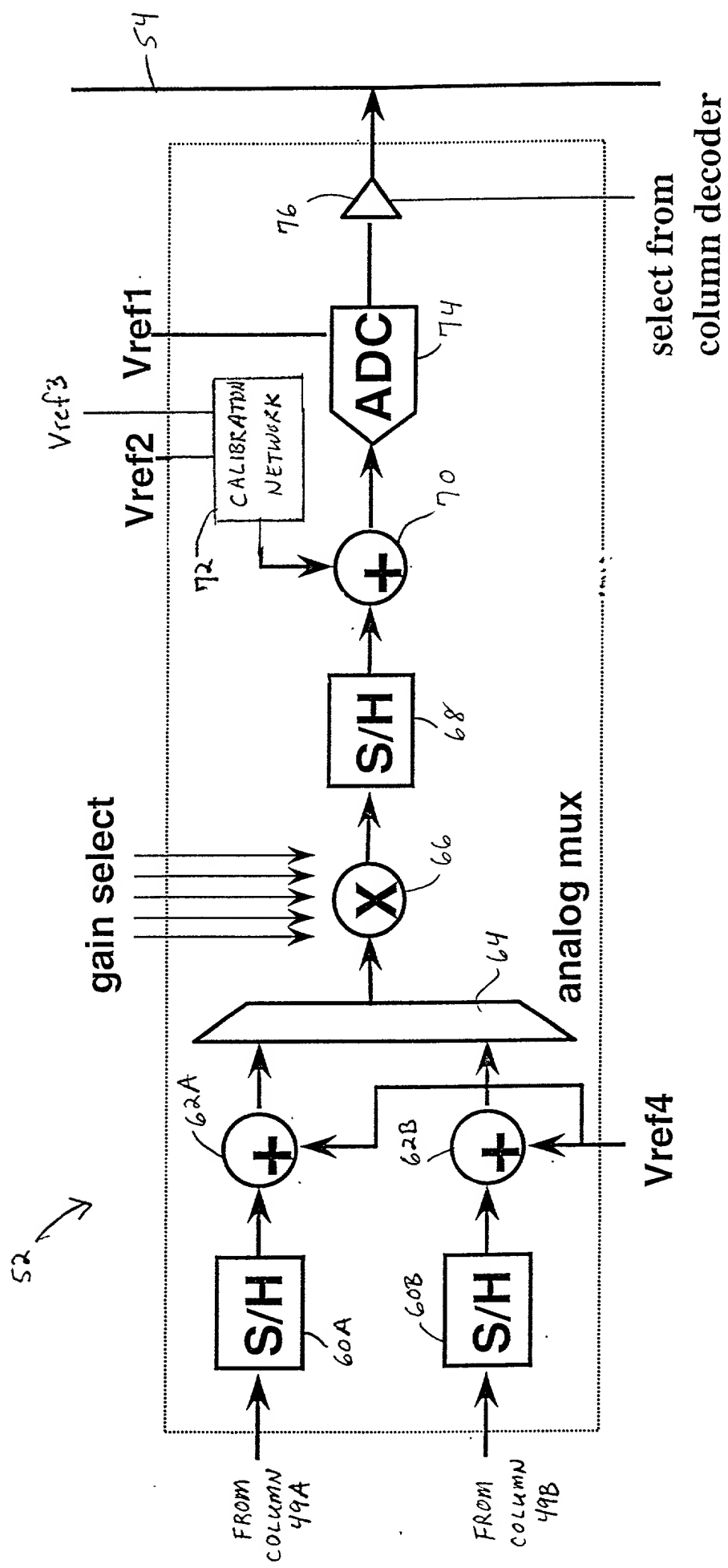
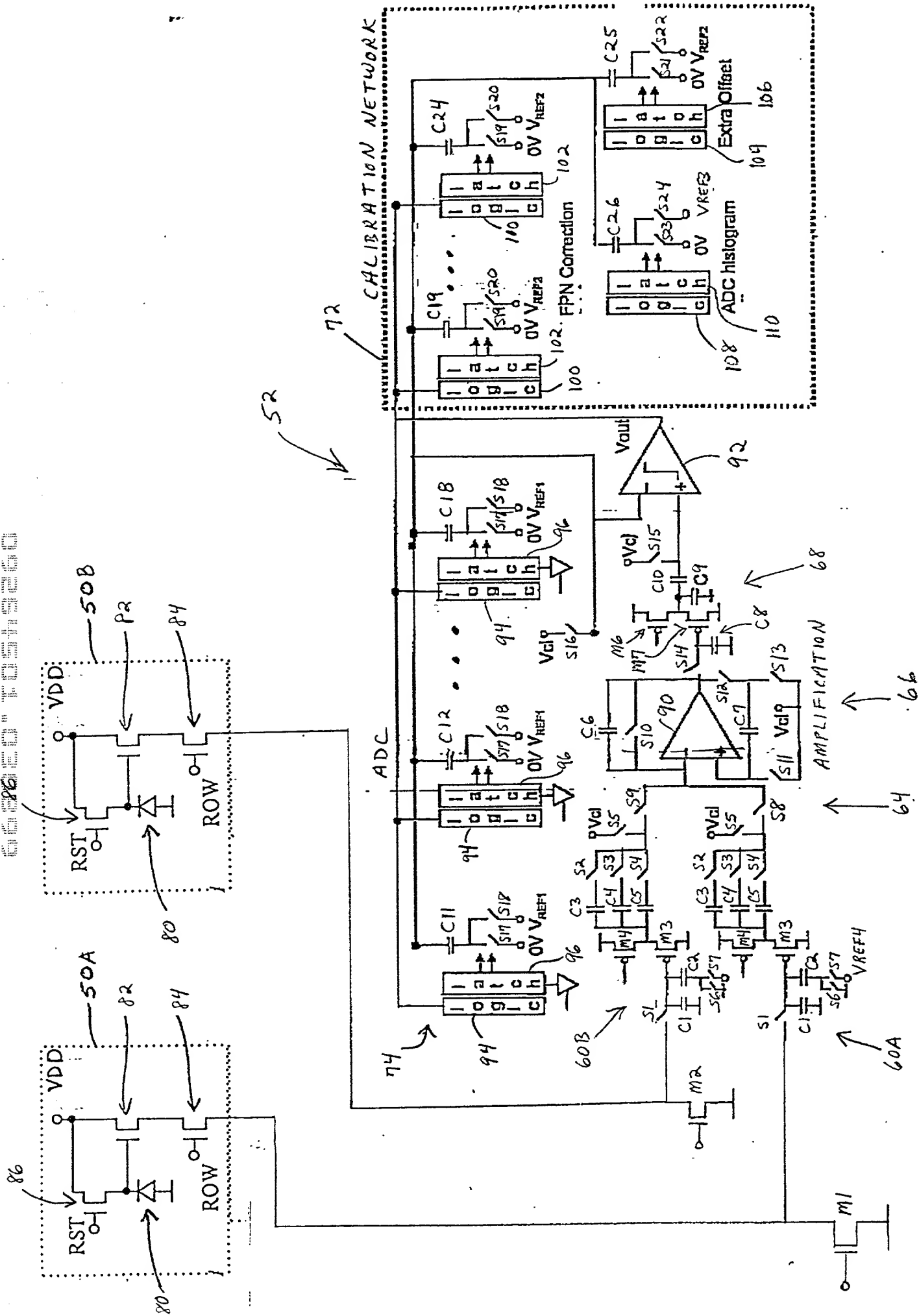


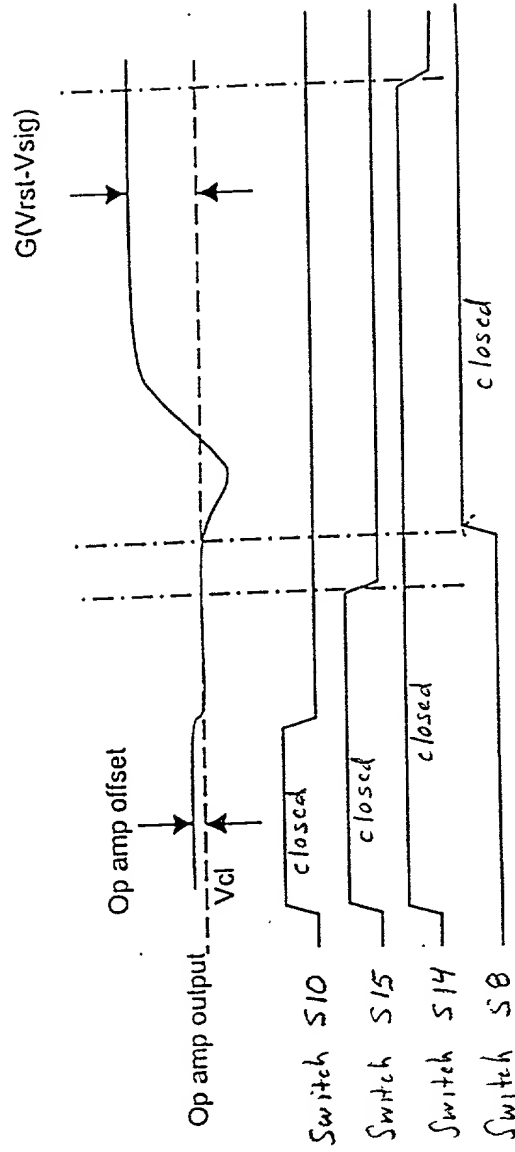
FIG. 3



Timing diagram for a 1T1C pixel circuit. The signals shown are:

- Pixel Output
- V_{signal}
- V_{reset}
- Input to amplification stage
- Photogate for selected row
- RST for selected row
- Switch S5
- Switch S1

Fig. 5



Amplification Timing

FIG. 7

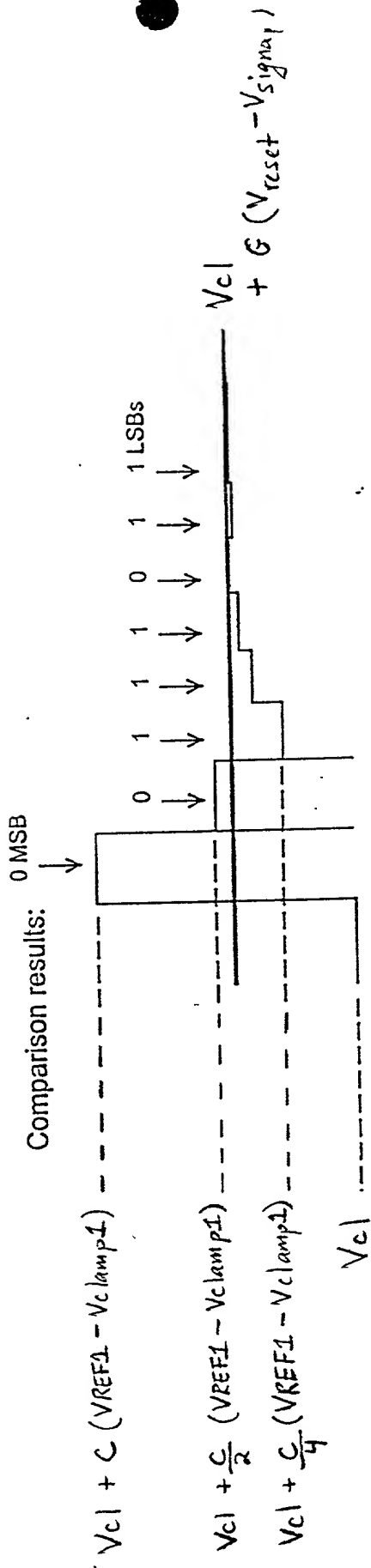


FIG. 9

To negative terminal
of comparator 92

$C11$

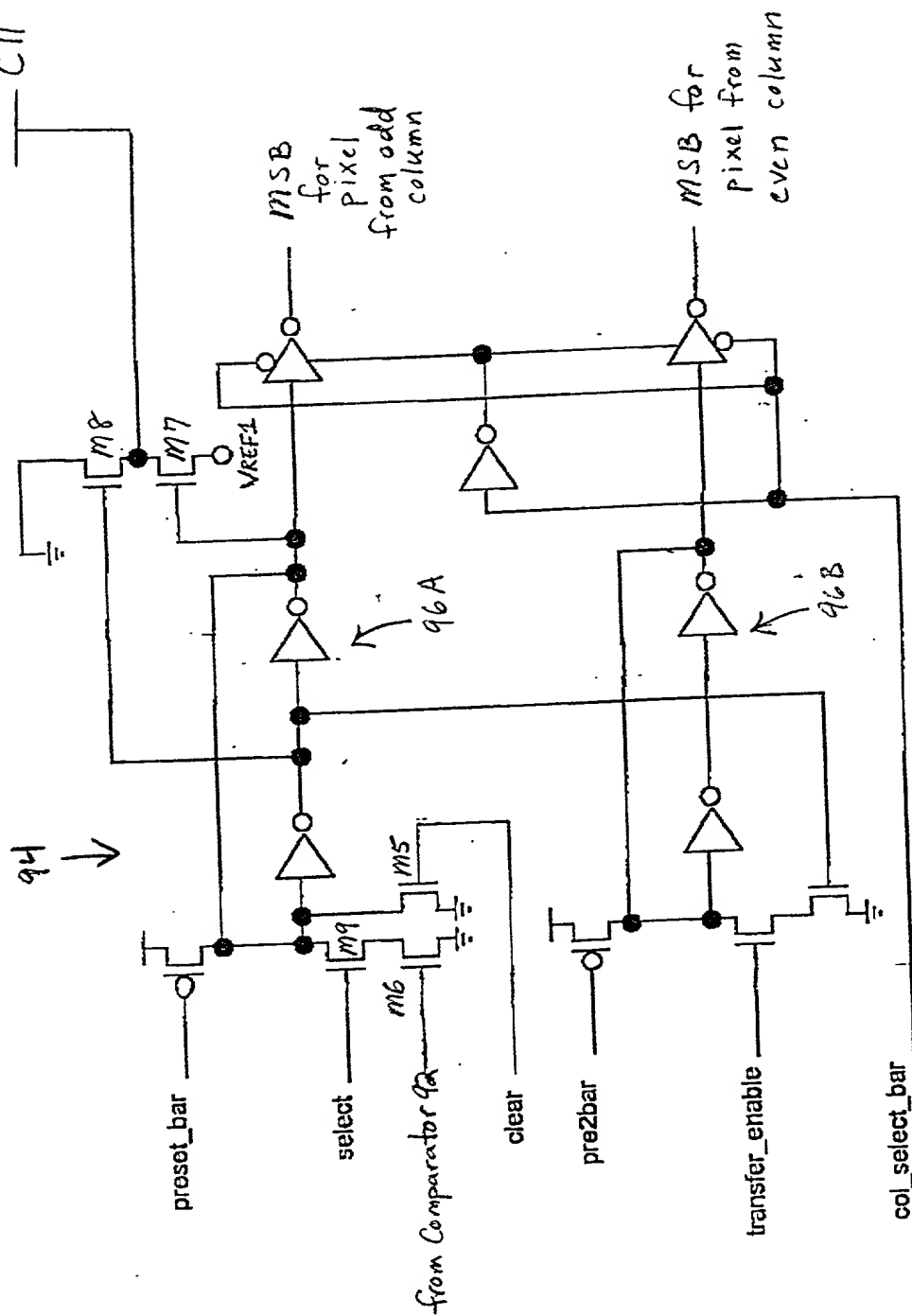
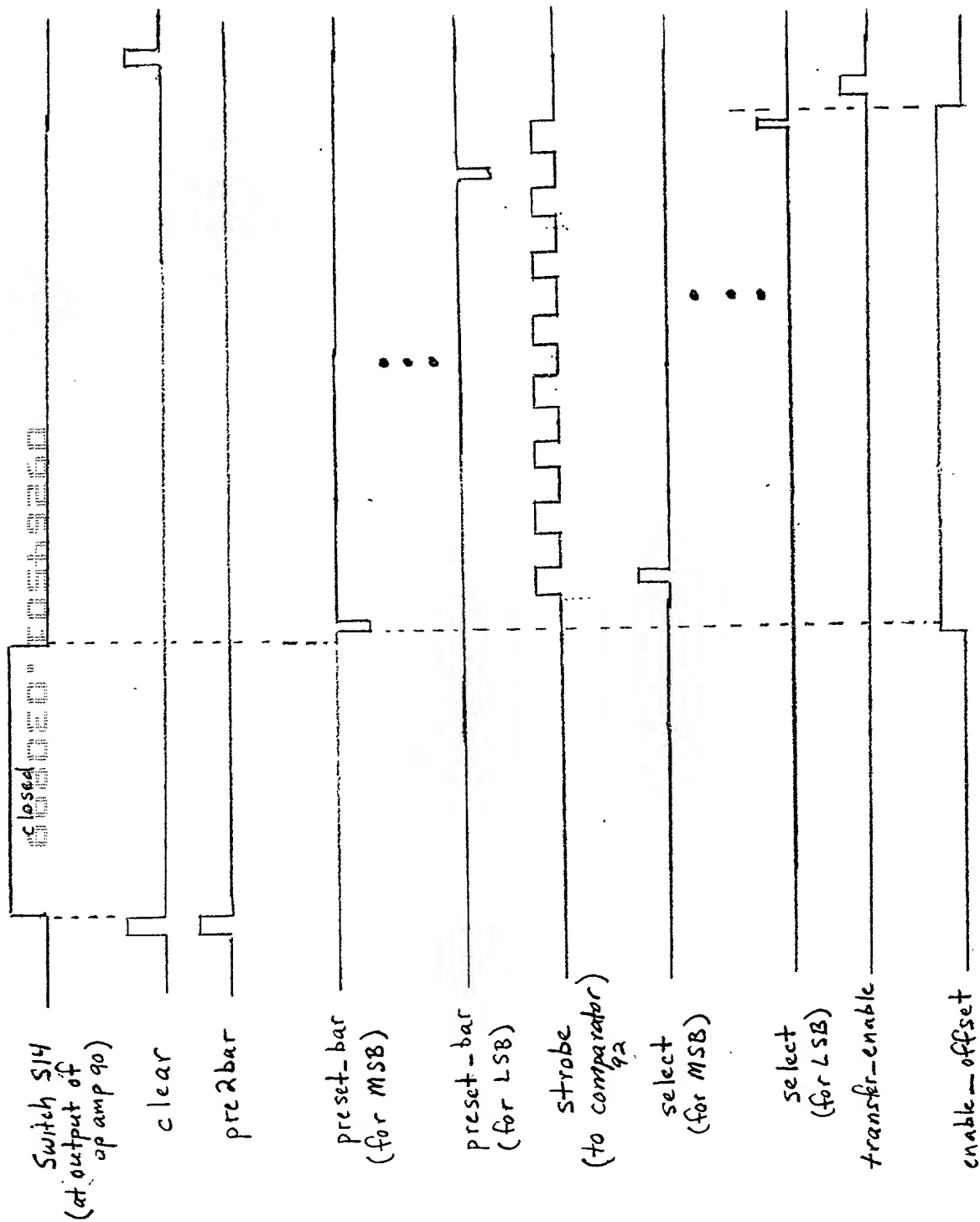


FIG. 10



← AMPLIFICATION → ANALOG-TO-DIGITAL CONVERSION →

FIG. 11

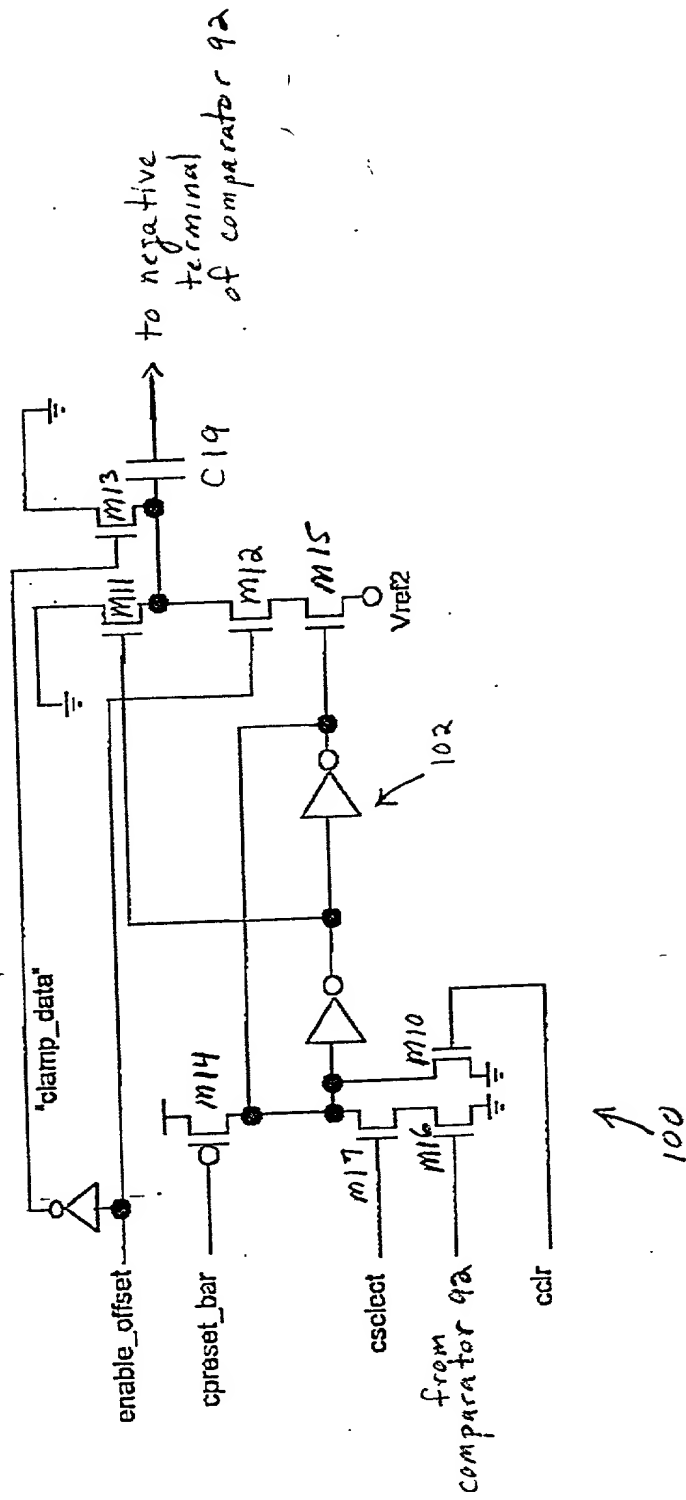
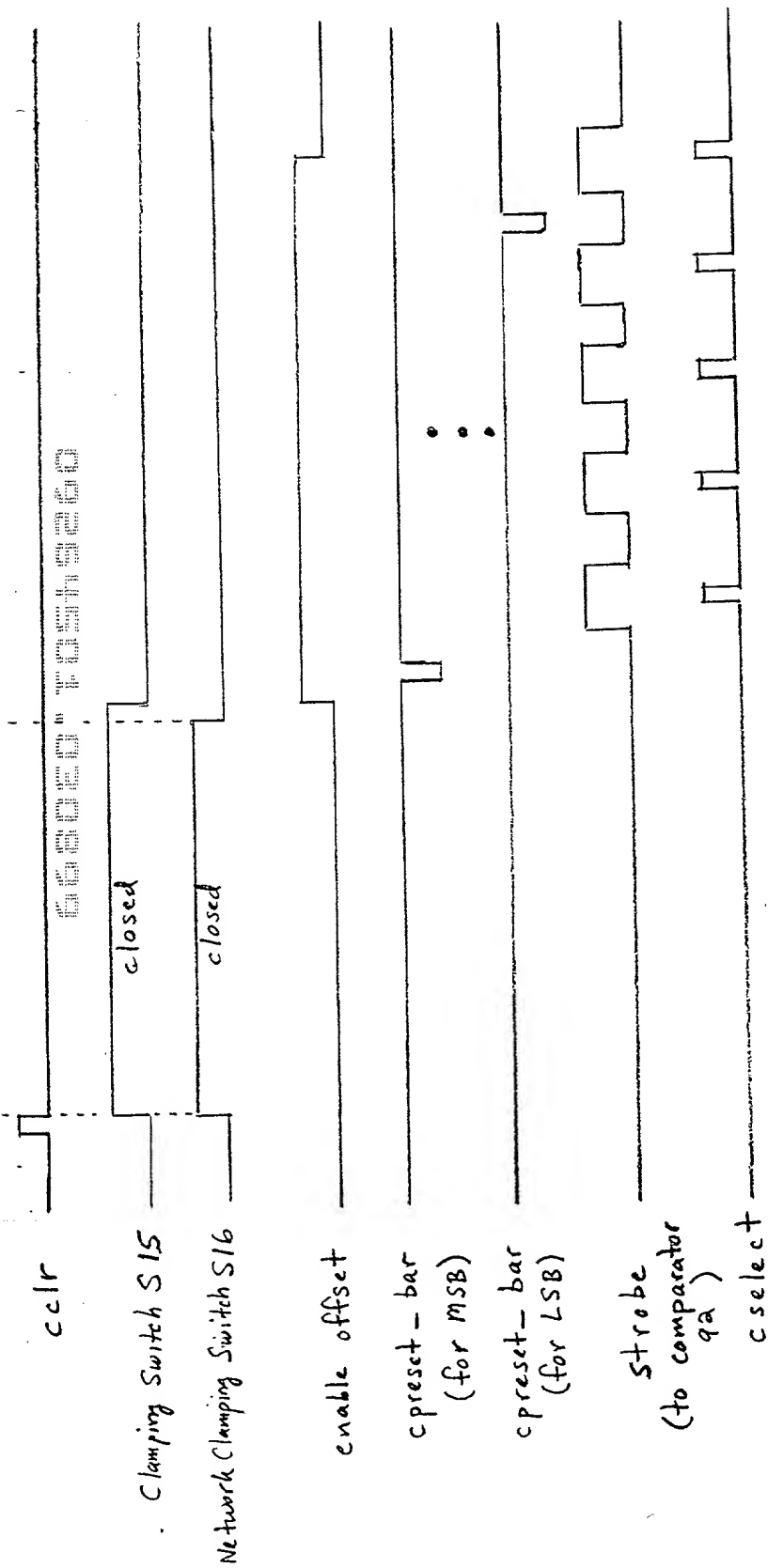


FIG. 12



CALIBRATION TIMING

FIG. 13

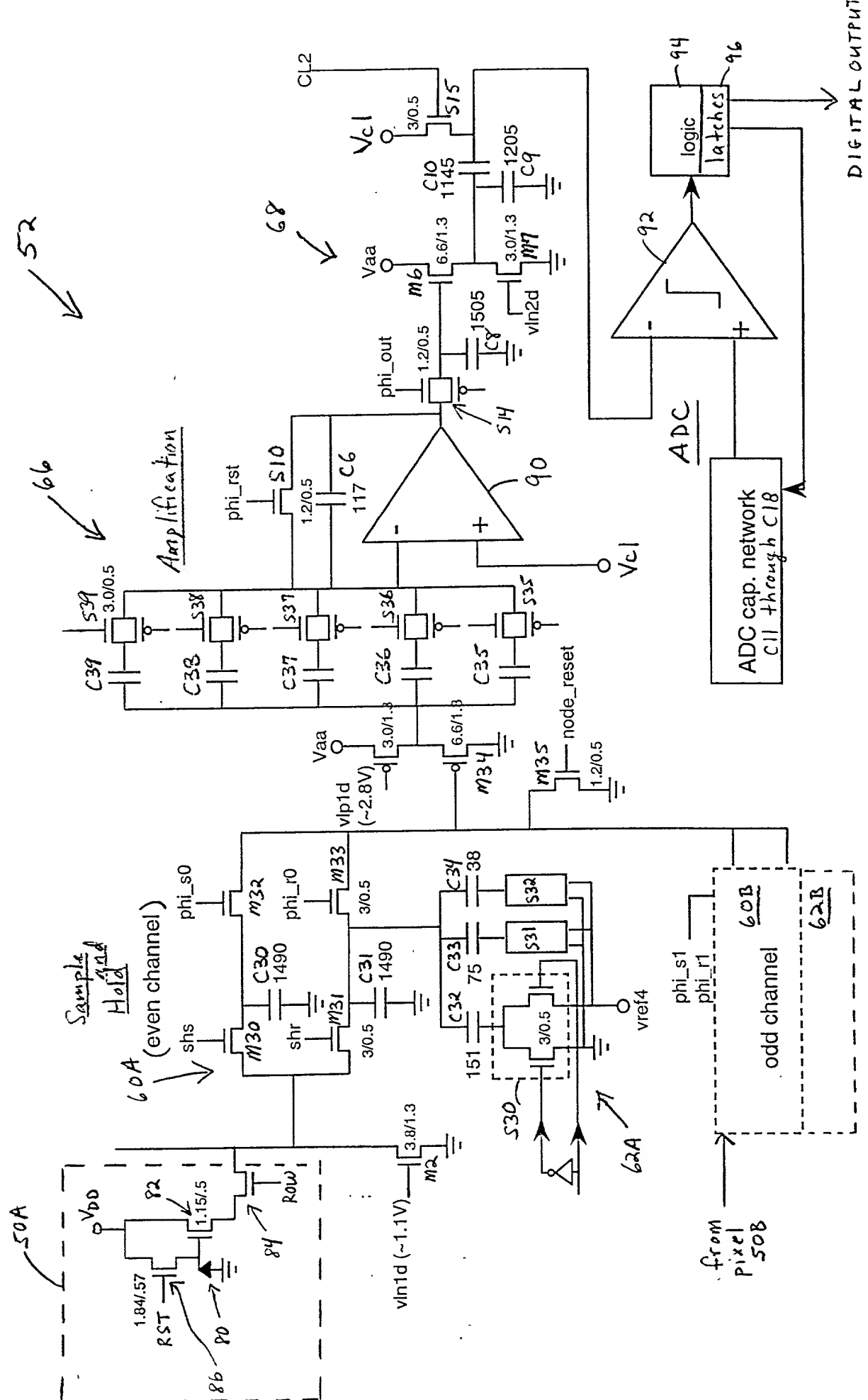


FIG. 14

pixel timing

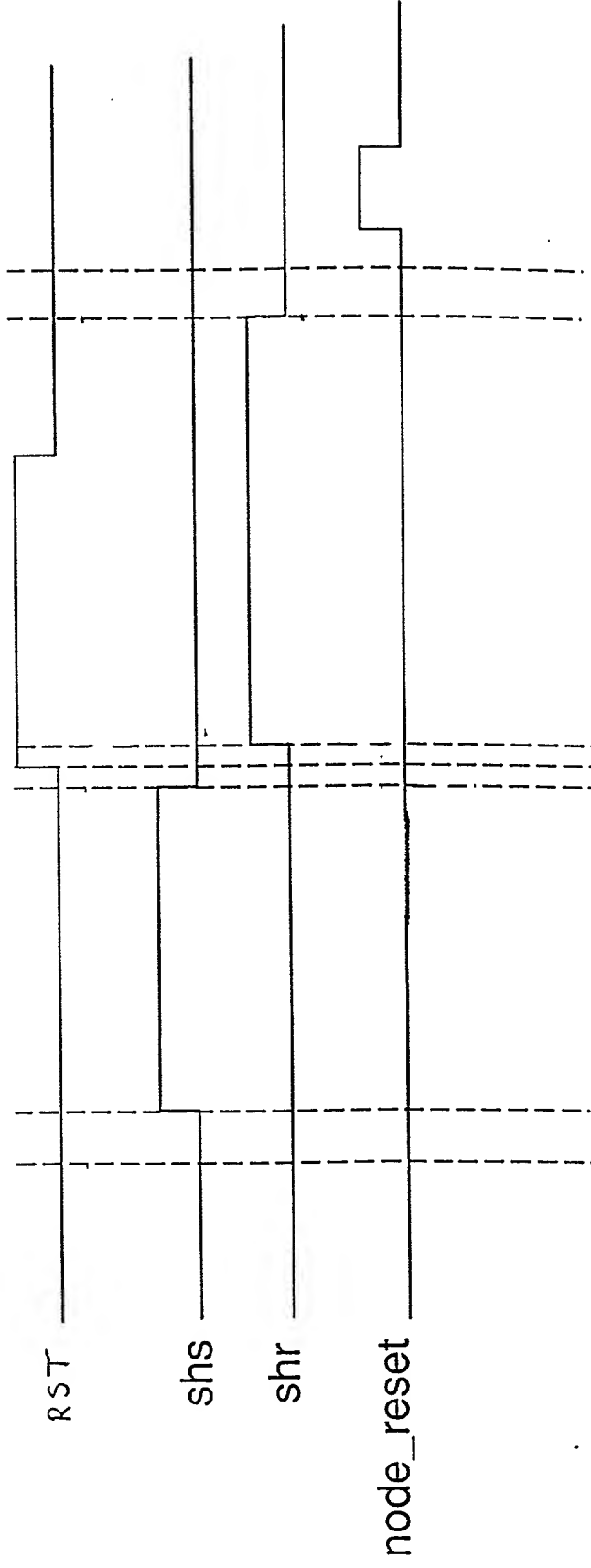


FIG. 15

gain timing

FIG. 16

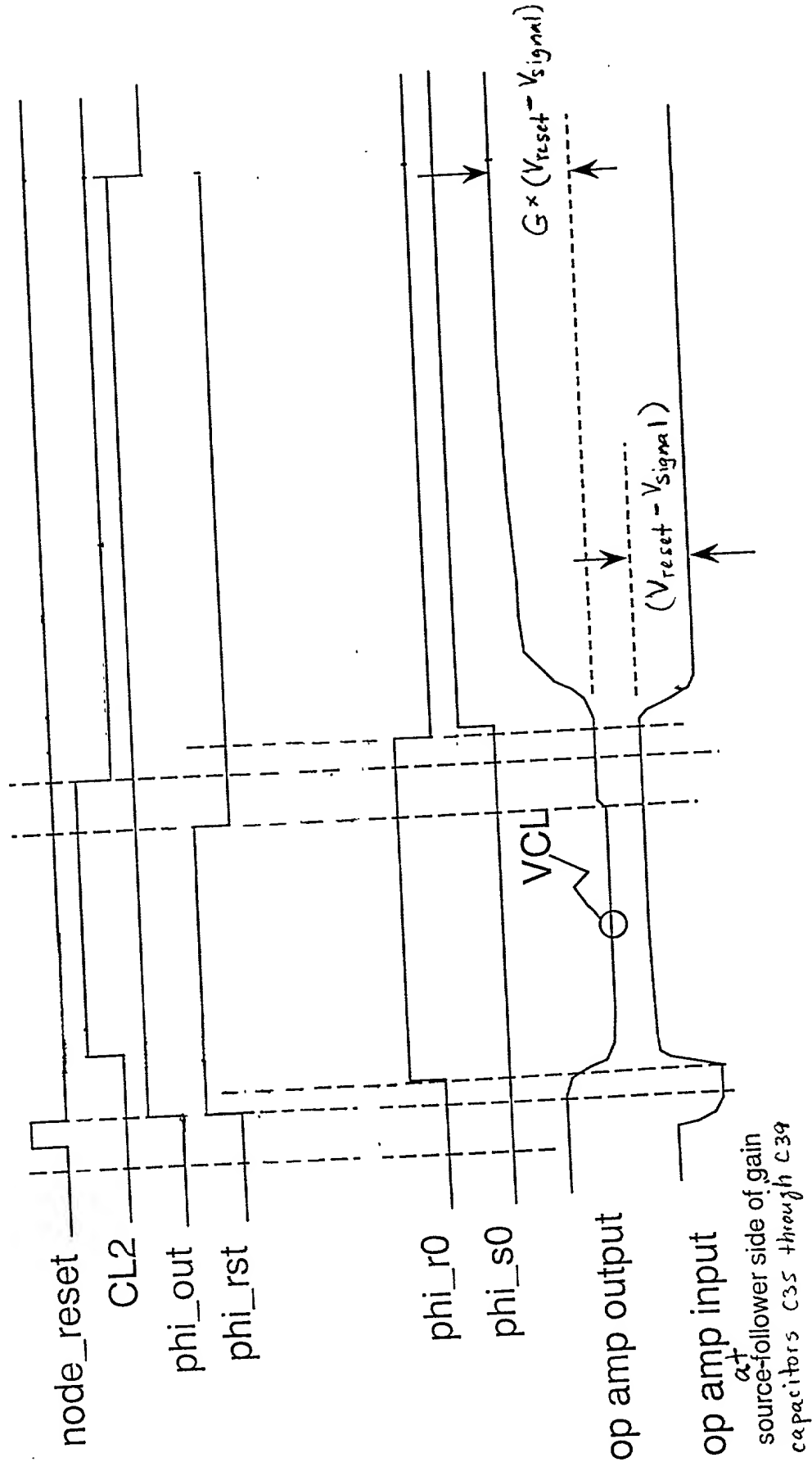


FIG. 16

COMBINED DECLARATION AND POWER OF ATTORNEY

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name,

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled READOUT CIRCUIT WITH GAIN AND ANALOG-TO-DIGITAL CONVERSION FOR IMAGE SENSOR, the specification of which

- ☒ is attached hereto.
☐ was filed on _____ as Application Serial No. _____
and was amended on _____.
☐ was described and claimed in PCT International Application No. _____
filed on _____ and as amended under PCT Article 19 on _____.

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose all information I know to be material to patentability in accordance with Title 37, Code of Federal Regulations, §1.56.

I hereby claim the benefit under Title 35, United States Code, §119(e)(1) of any United States provisional application(s) listed below:

U.S. SERIAL NO.	FILING DATE	STATUS
<u>60/077,599</u>	<u>March 9, 1998</u>	<u>PENDING</u>

I hereby appoint the following attorneys and/or agents to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith: Scott C. Harris, Reg. No. 32,030; William J. Egan, III, Reg. No. 28,411; David L. Feigenbaum, Reg. No. 30,378; John F. Land, Reg. No. 29,554; Ralph A. Mittelberger, Reg. No. 33,195; Hans R. Troesch, Reg. No. 36,950; John R. Wetherell, Jr., Reg. No. 31,678; Bing Ai, Reg. No. 43,312; George Pappas, Reg. No. 33,065; and Samuel Borodach, Reg. No. 38,388, of Fish & Richardson P.C.

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patents issued thereon.

Full Name of First Inventor: Roger Panicacci

Inventor's Signature: Roger Panicacci

Date: 3/8/99

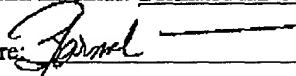
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COMBINED DECLARATION AND POWER OF ATTORNEY CONTINUED

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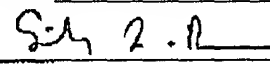
Date: 3/8/99

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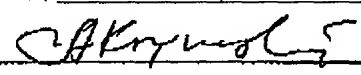
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